

MOKVELD, et al. - APPLICATION DATED: April 26, 2001

REMARKS

The specification has been amended to incorporate information regarding the priority application. Claims 2-10, 11 and 13 have been amended to correct minor idiomatic errors and to eliminate multiple dependency of the claims.

It is believed that the application is in condition for allowance. Accordingly, early and favorable notice of allowance of the present application is respectfully requested.

Respectfully submitted,

PILLSBURY WINTHROP LLP

By:

  
Paul L. Sharer

Reg. No. 36,004

Irina S. Zemel

Reg. No. 43,402

Tel. No.: (202) 861-3649

Fax No.: (202) 822-0944

1100 New York Ave., N.W.  
Ninth Floor - East Tower  
Washington, D.C. 20005  
(202) 861-3000

APPENDIX

VERSION WITH MARKINGS TO SHOW CHANGES MADE

IN THE SPECIFICATION:

The specification is changed as follows:

First full paragraph has been added.

IN THE CLAIMS:

**The claims are amended as follows:**

2. (Amended) Process for the production of a shaped article according to Claim 1, [characterized in that] wherein the polyolefin fibres are highly oriented polyethylene fibres having an intrinsic viscosity of at least 5 dl/g and a modulus of tension of at least 800 g/den.
3. (Amended) Process for the production of a shaped article according to Claim 1 [or Claim 2, characterized in that], wherein the solvent has been applied by distributing the solvent on one or more of the fibre layers before compression.
4. (Amended) Process for the production of a shaped article according to [any one of Claims 1-3, characterized in that] Claim 1, wherein the solvent has been applied as a result of the fibre layers containing solvent-containing polyolefin fibres with a solvent content of 0.02 – 25 wt.%.
5. (Amended) Process according to [any one of Claims 1-4, characterized in that] Claim 1, wherein the polyethylene fibres have a fineness of less than 5 denier per

filament.

6. (Amended) Process according to [any one of Claims 1-5, characterized in that] Claim 1, wherein the fibre layers contain unidirectionally oriented fibres and at most 30 wt.% matrix (relative to the total weight of the fibre layer), the direction of the fibres in the fibre layers being at an angles relative to that of the neighbouring fibre layers.
7. (Amended) Process for the production of an anti-ballistic shaped article according to [any one of Claims 1-6, characterized in that] Claim 1, wherein the solvent content is 0.05 – 5 wt.%.
8. (Amended) Process for the production of an anti-ballistic shaped article according to [any one of Claims 1-7, characterized in that] Claim 1, wherein the chi-parameter of the solvent relative to polyethylene (at 289 °K) is less than 0.5.
9. (Amended) Process for the production of an anti-ballistic shaped article according to [any one of Claims 1-8, characterized in that] Claim 1, wherein the solvent is a non-volatile paraffin.
10. (Amended) Process for the production of an anti-ballistic shaped article according to [any one of Claims 1-8, characterized in that] Claim 1, wherein compression is carried out at a pressure which is higher than 165 bar, at a compression temperature which is higher than 125°C and that the solvent content is 0.05 – 5 wt.%.
11. (Amended) Shaped article [obtainable] obtained according to a process of [any one of Claims 1-10] Claim 1.
13. (Amended) Shaped article according to Claim 11 [or Claim 12, characterized in that], wherein the SEA on impact of an AK47 MSC point is at least 115 J/kg/m<sup>2</sup>.

**MOKVELD, et al. - APPLICATION DATED: April 26, 2001**

**Claim 15 has been cancelled.**

Parameter	Value	Unit
1. $\alpha$	0.001	
2. $\beta$	0.001	
3. $\gamma$	0.001	
4. $\delta$	0.001	
5. $\epsilon$	0.001	
6. $\zeta$	0.001	
7. $\eta$	0.001	
8. $\theta$	0.001	
9. $\iota$	0.001	
10. $\kappa$	0.001	
11. $\lambda$	0.001	
12. $\mu$	0.001	
13. $\nu$	0.001	
14. $\xi$	0.001	
15. $\omicron$	0.001	
16. $\pi$	0.001	
17. $\rho$	0.001	
18. $\sigma$	0.001	
19. $\tau$	0.001	
20. $\upsilon$	0.001	
21. $\phi$	0.001	
22. $\chi$	0.001	
23. $\psi$	0.001	
24. $\omega$	0.001	
25. $\kappa$	0.001	
26. $\lambda$	0.001	
27. $\mu$	0.001	
28. $\nu$	0.001	
29. $\xi$	0.001	
30. $\omicron$	0.001	
31. $\pi$	0.001	
32. $\rho$	0.001	
33. $\sigma$	0.001	
34. $\tau$	0.001	
35. $\upsilon$	0.001	
36. $\phi$	0.001	
37. $\chi$	0.001	
38. $\psi$	0.001	
39. $\omega$	0.001	
40. $\kappa$	0.001	
41. $\lambda$	0.001	
42. $\mu$	0.001	
43. $\nu$	0.001	
44. $\xi$	0.001	
45. $\omicron$	0.001	
46. $\pi$	0.001	
47. $\rho$	0.001	
48. $\sigma$	0.001	
49. $\tau$	0.001	
50. $\upsilon$	0.001	
51. $\phi$	0.001	
52. $\chi$	0.001	
53. $\psi$	0.001	
54. $\omega$	0.001	
55. $\kappa$	0.001	
56. $\lambda$	0.001	
57. $\mu$	0.001	
58. $\nu$	0.001	
59. $\xi$	0.001	
60. $\omicron$	0.001	
61. $\pi$	0.001	
62. $\rho$	0.001	
63. $\sigma$	0.001	
64. $\tau$	0.001	
65. $\upsilon$	0.001	
66. $\phi$	0.001	
67. $\chi$	0.001	
68. $\psi$	0.001	
69. $\omega$	0.001	
70. $\kappa$	0.001	
71. $\lambda$	0.001	
72. $\mu$	0.001	
73. $\nu$	0.001	
74. $\xi$	0.001	
75. $\omicron$	0.001	
76. $\pi$	0.001	
77. $\rho$	0.001	
78. $\sigma$	0.001	
79. $\tau$	0.001	
80. $\upsilon$	0.001	
81. $\phi$	0.001	
82. $\chi$	0.001	
83. $\psi$	0.001	
84. $\omega$	0.001	
85. $\kappa$	0.001	
86. $\lambda$	0.001	
87. $\mu$	0.001	
88. $\nu$	0.001	
89. $\xi$	0.001	
90. $\omicron$	0.001	
91. $\pi$	0.001	
92. $\rho$	0.001	
93. $\sigma$	0.001	
94. $\tau$	0.001	
95. $\upsilon$	0.001	
96. $\phi$	0.001	
97. $\chi$	0.001	
98. $\psi$	0.001	
99. $\omega$	0.001	
100. $\kappa$	0.001	